Medial Knee Injury

Part 2, Load Sharing Between the Posterior Oblique Ligament and Superficial Medial Collateral Ligament

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Background: There is limited information regarding directly measured load responses of the posterior oblique and superficial medial collateral ligaments in isolated and multiple medial knee ligament injury states.

Hypotheses: Tensile load responses from both the superficial medial collateral ligament and the posterior oblique ligament would be measurable and reproducible, and the native load-sharing relationships between these ligaments would be altered after sectioning of medial knee structures.

Study Design: Descriptive laboratory study.

Methods: Twenty-four nonpaired, fresh-frozen adult cadaveric knees were distributed into 3 sequential sectioning sequences. Buckle transducers were applied to the posterior oblique ligament and the proximal and distal divisions of the superficial medial collateral ligament; 10 N·m valgus moments and 5 N·m internal and external rotation torques were applied at 0°, 20°, 30°, 60°, and 90° of knee flexion.

Results: With an applied valgus and external rotation moment, there was a significant load increase on the posterior oblique ligament compared with the intact state after sectioning all other medial knee structures. With an applied external rotation torque, there was a significant load decrease on the proximal division of the superficial medial collateral ligament from the intact state after sectioning all other medial knee structures. With an applied external rotation torque, the distal division of the superficial medial collateral ligament experienced a significant load increase from the intact state after sectioning the posterior oblique ligament and the meniscofemoral division of the deep medial collateral ligament.

Conclusion: This study found alterations in the native load-sharing relationships of the medial knee structures after injury. Sectioning both the primary and secondary restraints to valgus and internal/external rotation of the knee alters the intricate load-sharing relationships that exist between the medial knee structures.

Clinical Significance: In cases in which surgical repair or reconstruction is indicated, consideration should be placed on repairing or reconstructing all injured medial knee structures to restore the native load-sharing relationships among these medial knee structures.

Keywords: superficial medial collateral ligament; deep medial collateral ligament; posterior oblique ligament; sequential sectioning; buckle transducers

Injuries to the medial knee structures, often inaccurately referred to as injuries to the medial collateral ligament (MCL), are the most common knee ligament injuries. A complete understanding of medial knee biomechanics is necessary to assess which structures are to be given consideration when performing a repair or reconstruction. There are a number of quantitative biomechanical studies that have increased the knowledge of medial knee
structure function. Previous sequential sectioning studies have provided information regarding either the amount of increased motion or the decreased external applied force required to produce abnormal motion in ligament-deficient knees. However, both of these study designs are indirect measures of the compensatory load-sharing characteristics of the individual medial knee structures in injury states and do not provide individualized information for each individual ligament or its relationship to associated ligaments during injury.

Because of the indirect measurement methods used in these previous studies, a complete understanding of the complex interaction of the medial knee structures has not been fully attained. Our previous study directly measured the tensile forces on the intact medial knee structures for this same group of knees during external force application. Directly measuring the compensatory loads in medial knee structures in an injury state would provide insight into the clinical importance of repairing or reconstructing medial knee structures and understanding of the cause of graft failure in combined injury patterns.

The purpose of this study was to comprehensively examine the abnormal motion and load redistribution associated with injury to medial knee structures. In part 1 of this study, we quantified the roles that the posterior oblique ligament (POL), the proximal and distal divisions of the superficial MCL (sMCL), and the meniscofemoral and meniscotibial divisions of the deep MCL (dMCL) have in providing primary and secondary stabilization roles to valgus, external rotation, and internal rotation for the medial knee after sequential sectioning of medial knee structures. In part 2 of this study (this article), our purpose was to examine the compensatory load-sharing characteristics of the POL and the 2 divisions of the sMCL after sequential sectioning of the POL, the proximal and distal divisions of the sMCL, and the meniscofemoral and meniscotibial divisions of the dMCL. Our hypothesis was that tensile load responses from both the sMCL and the POL would be individually measurable and that the native load-sharing relationships between these ligaments would be altered after sectioning of medial knee structures.

MATERIALS AND METHODS

Specimen Preparation

Twenty-four nonpaired, fresh-frozen cadaveric knees with no evidence of prior injury with a mean age of 69.5 years (range, 45-87 years) were used for parts 1 and 2. The femur was potted in polymethylmethacrylate 20 cm proximal to the knee joint, and the tibia was sectioned 12.5 cm distal to the knee joint. A threaded rod was inserted into the tibial intramedullary cavity, parallel with the long axis of the tibia, and fixed in position with polymethylmethacrylate. A hexagonal lock nut was attached to the tibial rod to allow for application of external loads.

The knee-testing apparatus firmly secured the femur at a horizontal angle, while allowing uninhibited movement of the tibia at the measured knee flexion angles. After the knee was aligned in the testing apparatus, buckle transducers were securely fastened to the POL, the proximal division of the sMCL, and the distal division of the sMCL (Figure 1).

Observed Ligament Load via Buckle Transducers

The buckle transducers consisted of a crossbar and a rectangular frame containing semiconductor strain gauges. The use of these devices has been previously described in detail. Surrounding bone or soft tissue impingement of the buckle frames and undesirable ligament damage during biomechanical testing were minimized by using crossbars of assorted depths. The buckle transducer application consisted of placing the frame over the ligament of interest and inserting the crossbar both below the ligament and above the frame. Therefore, ligament tension, caused by loading of the specific ligament, pushed the crossbar against the frame, similar to 3-point bending. Deformation of the buckle frame induced a voltage response in the strain gauge contained within the buckle frame. Finally, this voltage output was relayed to a data acquisition system. Prior work has reported that there is a linear relationship between applied load and voltage output. Therefore, the voltage outputs were converted to kilonewtons according to a conversion factor determined by posttest calibration.

References

1. References 1, 4, 9, 10, 13, 24, 25, 28, 30, 31, 33.
2. References 2, 3, 22, 27, 29, 32, 35, 36.
of each buckle with a known load. Buckles were zeroed before each external load application to ensure accurate load measurements. Buckle transducers have been reported to be repeatable to within 0.7% using a similar biomechanical testing protocol.\textsuperscript{19}

**External Force Application**

Each knee was tested at 0°, 20°, 30°, 60°, and 90° of knee flexion. Knees were randomly assigned to 3 sequential sectioning sequences with a total of 8 knees per sequence (Table 1). The sequences involved sectioning of the POL, the proximal and distal divisions of the sMCL, and the meniscofemoral and meniscotibial divisions of the dMCL (Figure 2). A 100-N force model SM S-type load cell (Interface, Scottsdale, Arizona; manufacturer reported nonrepeatability error of ±0.01%) was used to apply a 10-N m valgus moment on the tibial rod 22.9 cm distal to the joint line; 5-N m external and internal rotation torques were applied to the lock nut on the tibial rod with a 15-N m capacity model TS12 shaft style reaction torque transducer (Interface, manufacturer reported nonrepeatability error of ±0.02%). Varus moments were not applied to the knee because pilot testing of 3 specimens revealed no load responses from these structures during the application of a 10-N m varus moment. Before experimental testing, the load cell and torque transducer were calibrated to establish a linear relationship between voltage output and force application. For each sequential sectioning series and flexion angle, external loads were applied to the specimen 3 times and the results averaged.

**Data Analysis**

Ligament tensile forces during testing were determined by calibrating the measured buckle voltages against a standardized load. After sectioning of a ligament, the buckle of interest was calibrated by directly tensioning the ligament using a load cell according to a previously described method.\textsuperscript{6,20}

Voltage measurements during biomechanical testing were simultaneously collected from the buckle transducers and the previously described torque transducer or load cell. When the external force applied to the structure equaled the target force, the correlating buckle voltage outputs were converted to force measurements according to the previously defined linear regression outlined above. These force measurements were indicative of the tensile load response in the ligament of interest.

**Statistical Analysis**

A 2-way analysis of variance was used to compare each particular ligament’s load response to valgus loads and internal and external rotation torques for each particular flexion angle between sectioned states. Tukey’s honestly significant difference was used for post hoc comparisons to detect significant differences between particular pairs of the load responses considered in each analysis of variance. A significant difference was determined to be present for \( P < .05 \).

**RESULTS**

**Force on the POL**

Compared with the intact state, there was a significant load increase to an applied valgus moment on the POL after sectioning the proximal and distal divisions of the sMCL and the meniscofemoral and meniscotibial divisions of the dMCL at 0° (14.9 vs 24.3 N), 20° (12.0 vs 28.3 N), and 30° (12.0 vs...
26.4 N) of knee flexion ($P < .05$) (Figure 3). There was also a significant increase in load on the POL with an applied external rotation torque after sectioning both divisions of the sMCL and the dMCL at 60° (11.7 vs 13.0 N, $P < .05$) of knee flexion.

Forces on the Proximal Division of the sMCL

Compared with the intact state, there was a significant load decrease to an applied external rotation torque on the proximal division of the sMCL after sectioning the POL, meniscofemoral and meniscotibial divisions of the dMCL, and distal division of the sMCL at 30° (48.6 vs 19.0 N, $P < .05$) and 90° of knee flexion (54.3 vs 15.9 N, $P < .05$) (Figure 4).

Force on the Distal Division of the sMCL

Compared with the intact state, there was a significant load increase to an applied valgus load on the distal division of the sMCL after sectioning the dMCL at 90° of knee flexion (75.4 vs 78 N, $P < .05$). With an applied external rotation load, there was a significant load increase seen on the distal division of the sMCL at 0° and 20° of knee flexion after sectioning the POL and the meniscofemoral division of the dMCL ($P < .05$) (Figure 5). With an applied internal rotation load, there was a significant load increase after sectioning the POL and meniscofemoral and meniscotibial divisions of the dMCL at 20° of knee flexion seen on the distal division of the sMCL from the intact state (25.6 vs 38.8 N, $P < .05$).

DISCUSSION

Our unique experimental setup allowed us to directly measure the changes in tensile force experienced by ligaments in an injury state. This information is useful because it identifies alterations in the native load-sharing relationships of medial knee structures after injury. Furthermore, our multiple sectioning sequences allowed us to demonstrate the effects resulting from injury to secondary stabilizers when the primary stabilizers were intact. Our previous study directly measured and reported on the tensile loads experienced by the POL and the 2 divisions of the sMCL in the intact knee on the same knees as this study. This previous study quantitatively reported on the distinct importance of the distal division of the sMCL in
response to valgus moments and the previously underesti-
timated function of the POL in resisting internal rotation
forces at knee flexion angles close to extension.6

The anatomy of the sMCL is well described in the
literature.3,15,18,34 It has an attachment to the femur
proximoposterior to the medial epicondyle,15,25 a proximal
tibial attachment on the soft tissue medial to the ante-
rior arm of the semimembranosus,3,15 and a distal tibial
bone attachment anterior to the posteromedial crest of
the tibia.15,25 These 3 attachment sites divide the func-
tional anatomy of the sMCL into a proximal and a distal
division.

Although the proximal tibial attachment is a readily
identifiable structure, this primarily soft tissue attach-
ment is not as static as either the femoral or distal tibial
attachments, which attach directly to bone. Furthermore, it
has been noted that the more superficial, or medial, fibers
of the sMCL do not attach to the proximal tibial attach-
ment. The distal division of the sMCL was reported to be a
primary knee stabilizer to external rotation in part 1 of this
2-part study. The difference in attachment site fixation
could be an explanation for the significant decrease in
external rotation load response that we observed in the
proximal sMCL division at 30° after sectioning of the other
medial knee structures. We theorize that as a result of the
primarily soft tissue attachment on the proximal tibia, the
proximal division of the sMCL was not statically tethered,
resulting in the significantly decreased load response to
external rotation. In addition, we theorize that the more
medial sMCL fibers, which do not attach directly to its
proximal tibial attachment, become less taut during exter-
nal rotation loads, resulting in the decrease in force seen
on the proximal division of the sMCL. Subsequently, the
increased load not absorbed by the proximal division of
the sMCL was likely diverted to a structure not measured in
this study, such as the dMCL or the cruciate ligaments.

With regard to the forces seen on the POL, we found a
significant increase in valgus load compared with the
intact state after sectioning the components of both the
dMCL and sMCL at 0°, 20°, and 30° of knee flexion. This
observation correlates both with a previous article that
demonstrated that the POL experiences tensile load to
valgus forces in intact knees especially close to knee exten-
sion3 and with the previous literature that reported the
POL has a secondary stabilization role in valgus stability
of the knee.8,28,34 Therefore, it is logical that the POL would
demonstrate an increased load response in sMCL- and
dMCL-deficient knees.

The limitations of this study include that we were only
able to apply buckle transducers to the POL and the prox-
imal and distal divisions of the sMCL. Because of the limita-
tions of buckle transducers, we were not able to apply them
to the meniscofemoral and meniscotibial portions of the
dMCL because it would create impingement by the sMCL,
which would result in inaccurate readings for these struc-
tures. In addition, we did not apply buckle transducers to
other supporting knee structures and thus were not able to
measure which structures took up the additional load seen
with specific structure sectioning. We did not anticipate our
findings of a decrease in load for the proximal division of
the sMCL with external rotation loading with sectioning of
other structures. Although we theorize this decrease in
measured load on the proximal division was owing to the
lack of stability provided by the more medial fibers becom-
ing untethered with external rotation loads due to the dis-
tal attachment being sectioned, it was possible that other
structures not measured in this study, such as the dMCL,
may have taken up this load.

Our results add to part 1 with load information pertain-
ing to an increase in motion after sectioning. Our results
demonstrated that medial knee injuries alter the intricate
load-sharing relationships that exist between all of the
medial knee structures, which, if left untreated, could
potentially increase the risk for further injury. Therefore,
in cases in which surgical repair or reconstruction is indi-
cated, consideration should be given to repairing or recon-
structing all injured medial knee structures to restore the
normal load-sharing relationships among these structures
at the time of surgical treatment.

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